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CIVIL ENGINEERING
INDIANA
DEPARTMENT OF HIGHWAYS

JOINT HIGHWAY RESEARCH PROJECT

FHWA/IN/JHRP-86/18

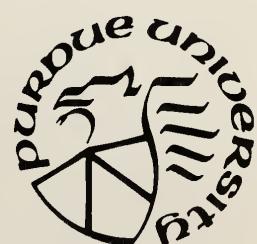
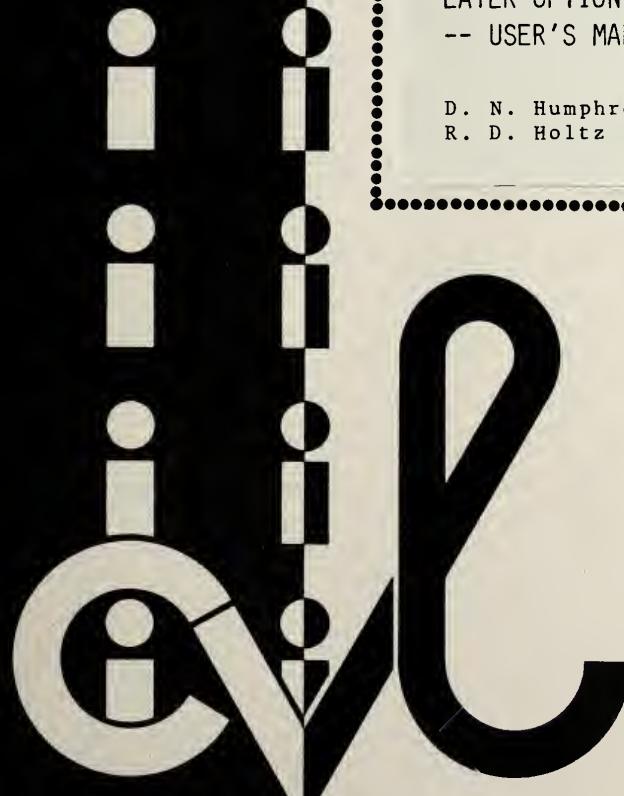
Implementation Report (2)

STABL6 WITH REINFORCING
LAYER OPTION

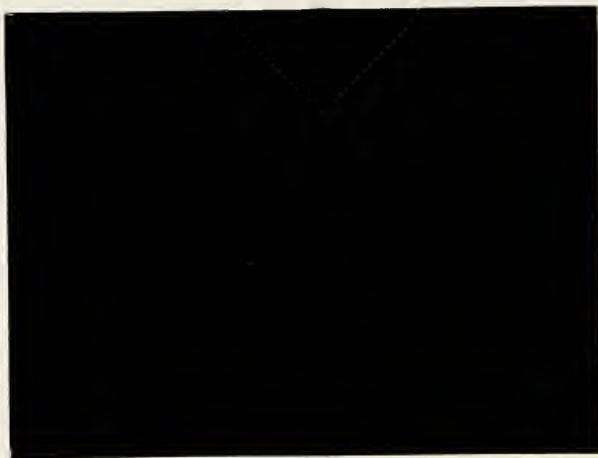
-- USER'S MANUAL --

D. N. Humphrey

R. D. Holtz



PURDUE UNIVERSITY



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FHWA/IN/JHRP-86/18
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D. N. Humphrey
R. D. Holtz



Implementation Report (2)

STABL6 WITH REINFORCING LAYER OPTION
-- USER'S MANUAL --

TO: H. L. Michael, Director
Joint Highway Research Project

FROM: R. D. Holtz, Research Engineer
Joint Highway Research Project

DATE: October 14, 1986

PROJECT: C-36-36Q

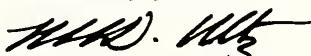
FILE: 6-14-17

Attached is a user's manual on the HPR Part II research study entitled "Design of Reinforced Embankments." This report, a user's manual, is the implementation part of Task 5 of the approved work plan. The authors of the report are Mr. D. N. Humphrey and myself.

The popular stability analysis program STABL, which can be used to analyze ordinary unreinforced embankments on soft foundations, was modified so that reinforced embankments also could be considered. The new program, termed STABL6, uses the simplified Bishop's analysis method, and it is implemented on IBM PC-compatible micro computers. The User's Manual gives detailed input instructions as well as an example problem which illustrates the analysis of a typical reinforced highway embankment. The report should be useful to highway designers who wish to utilize simple limiting equilibrium analysis methods for design purposes.

Copies of the report will be submitted to the IDOH and FHWA for their review. I look forward to receiving their comments on the manual.

Sincerely yours,



R. D. Holtz, Ph.D., P.E.
Research Engineer

RDH/kr

Attachment

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IMPLEMENTATION REPORT (2)

STABL6 WITH REINFORCING LAYER OPTION
-- USER'S MANUAL --

by

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Project No.: C-36-36Q

File No.: 6-14-17

Prepared as Part of an Investigation

Conducted by

Joint Highway Research Project
Engineering Experiment Station
Purdue University

in cooperation with the

Indiana Department of Highways

Purdue University
West Lafayette, Indiana

October 14, 1986



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1. Report No. FHWA/IN/JHRP-86/18	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle STABL6 WITH REINFORCING LAYER OPTION -- USER'S MANUAL		5. Report Date October 14, 1986
6. Performing Organization Code		
7. Author(s) D. N. Humphrey and R. D. Holtz		8. Performing Organization Report No. JHRP-86-18
9. Performing Organization Name and Address Joint Highway Research Project Civil Engineering Building Purdue University West Lafayette, IN 47907		10. Work Unit No.
		11. Contract or Grant No. HPR-1(24) Part II
		12. Type of Report and Period Covered Implementation Report
		13. Sponsoring Agency Code
14. Supplementary Notes Prepared in cooperation with the U.S. Department of Transportation, Federal Highway Administration. Study entitled "Design of Reinforced Embankments."		
15. Abstract The capability to analyze reinforced embankments has been incorporated into the STABL slope stability analysis program. The new program is called STABL6. This user's manual describes how the simplified Bishop's method was modified to include reinforcing layers. The modified program can analyze multiple reinforcing layers and allows the orientation of the reinforcing force to be specified. Input instructions and an example problem for the reinforcing layer option are given.		
17. Key Words Stability analysis, reinforcement, embankments, design, analysis, limiting equilibrium		18. Distribution Statement No restrictions. This document is available to the public through the National Technical Information Service, Springfield, Virginia 22161
19. Security Classif. (of this report) unclassified	20. Security Classif. (of this page) unclassified	21. No. of Pages 33
22. Price		



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HIGHLIGHT SUMMARY

The capability to analyze reinforced embankments has been incorporated into the STABL slope stability analysis program. The new program is called STABL6. This user's manual describes how simplified Bishop's method was modified to include reinforcing layers. The modified program can analyze multiple reinforcing layers and allows the orientation of the reinforcing force to be specified. Input instructions and an example problem for the reinforcing layer option are given.

PC-STABL6 WITH REINFORCING LAYER OPTION
-- USER'S MANUAL --

INTRODUCTION

A slope stability program PC-STABL5 developed at Purdue University was modified to give it the capability to analyze embankments constructed on soft ground reinforced with one or more layers of reinforcement. This modified program is called PC-STABL6. It was developed as part of a study of design of reinforced embankments (Humphrey and Holtz, 1986a) that also included a finite element analysis procedure (Humphrey and Holtz, 1986b). PC-STABL5 is a general purpose limiting equilibrium slope stability analysis program with solution options that use the simplified Janbu method with circular, sliding block, or irregular shaped sliding surfaces or the simplified Bishop or Spencer methods with circular surfaces. Program operation is described in Siegel (1975a), Lovell, et al. (1984), and Carpenter (1985). Further details on program development are given in Siegel (1975b) and Boutrup (1978). The program is written in FORTRAN77 and operates on IBM-PC, IBM-XT, IBM-AT, or compatible computers.

The simplified Bishop analysis routine was modified to include the stabilizing moment provided by one or more

layers of reinforcement. The user inputs the location of each layer, the distribution of available force, and the direction in which the force acts. The circular trial surface may be specified or PC-STABL5's surface generation routine may be used.

This report is a user's manual for analysis of reinforced embankments with PC-STABL6. Only aspects of the program specific to the reinforcement option are covered. The user is referred to the references noted above for general instructions on program use. In the following, the method used to incorporate the stabilizing effect of the reinforcing layer is described and an outline of the solution procedure is given. Appendix A lists references cited. Appendix B gives an example problem. The data input format is detailed in Appendix C. Error codes used by the reinforcing layer routines are given in Appendix D. Appendix E lists the modifications made to PC-STABL5 and two new subroutines that were added. Modifications to the routine to output problem geometry on a Hewlett-Packard 7470A two pen plotter are listed in Appendix F.

ANALYSIS OF REINFORCING LAYERS WITH SIMPLIFIED BISHOPS METHOD

Background

Tensile reinforcing layers provide a resisting moment which increases embankment stability. This effect was

incorporated into the simplified Bishop (1955) method of analysis. It was assumed that the reinforcement provides only a resisting moment and does not alter the stresses on the assumed slip surface. Finite element analyses confirmed that the reinforcement has an insignificant effect on normal stresses on the portion of the failure surface passing through the embankment (Humphrey and Holtz, 1986a). Furthermore, the soil strength and available reinforcing force are assumed to be mobilized simultaneously. The implications of this assumption should be critically examined when the foundation soils reach a peak shear strength at small strain followed by strain softening.

In the simplified Bishop method a circular shaped slip surface is assumed and divided into a number of slices. A slip surface and the forces acting on a typical slice are shown in Fig. 1. The reinforcing force F_R acting at the intersection of the slip surface and the reinforcement is also shown. F_R has units of force/unit width. It provides a resisting moment equal to F_R times its moment arm, y , about the center of the circle. If there are multiple reinforcing layers, the total resisting moment is the sum of the resisting moment provided by each layer. This additional resisting moment is included in the equation for the safety factor (Ingold, 1982; Humphrey and Holtz, 1986):

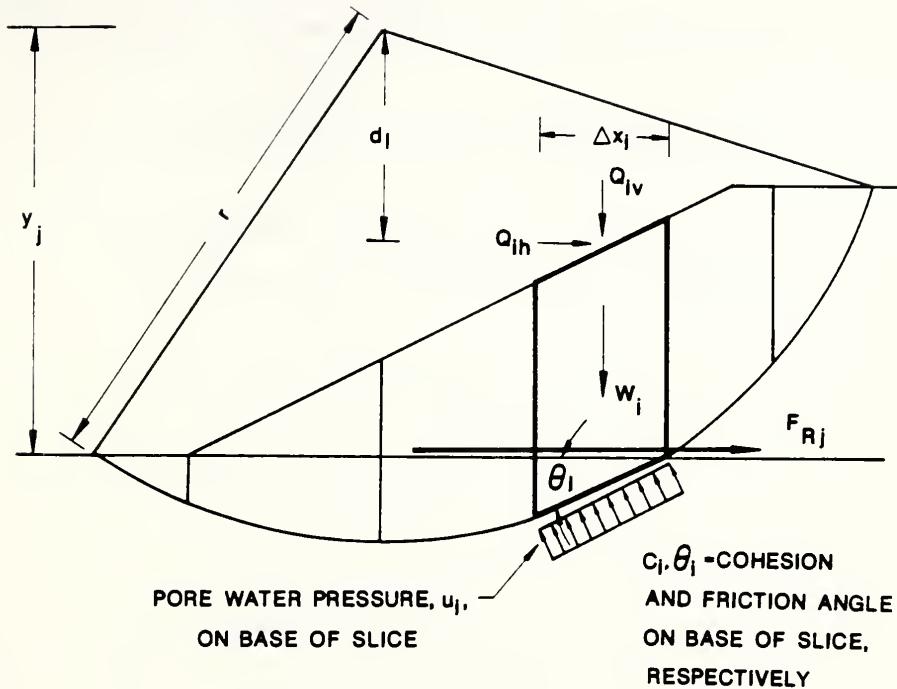


Figure 1 Simplified Bishop method of slices including horizontal reinforcing force showing forces acting on i^{th} slice.



$$SF = \frac{\sum_{i=1}^n \left[\frac{c_i \Delta x_i + [W_i + Q_{iv} - u_i \Delta x_i] \tan \phi_i}{\cos \theta_i + (\sin \theta_i \tan \phi_i) / SF} \right]}{\sum_{i=1}^n (W_i + Q_{iv}) \sin \theta_i - [\sum_{i=1}^n Q_i h d_i] / r - (\sum_{j=1}^m F_{Rj} y_j) / (r SF)} \quad (1)$$

where: W_i = weight of the i^{th} slice

Q_{iv} = vertical surface load applied to the i^{th} slice

Q_{ih} = horizontal surface load applied to the i^{th} slice

d_i = moment arm of Q_{ih}

u_i = pore water pressure acting on base of i^{th} slice

Δx_i = width of i^{th} slice

θ_i = inclination of base of i^{th} slice

c_i = cohesion on base of i^{th} slice

ϕ_i = friction angle on base of i^{th} slice

r = radius of assumed trial circle

n = number of slices

F_{Rj} = force in j^{th} reinforcing layer

y_j = moment arm for j^{th} reinforcing layer

m = number of reinforcing layers

SF = safety factor

The safety factor which satisfies Eq. 1 is found by trial and error. This equation was implemented in STABL5.



Implementation

To use the reinforcing option, the location of each layer is specified by a series of x,y coordinates starting at the left end of the reinforcement and moving to the right as shown in Fig. 2. In a typical application the left end of the layer would be at the embankment toe or the face of the slope and would extend across the full width of the embankment. The layer may be horizontal or inclined, however, the user must employ judgment on the applicability of the analysis method if the layers are more than moderately inclined. It is the user's responsibility to define a reasonable reinforcement geometry.

The available force and orientation of the force is specified at each point defining the reinforcing layer. Similar procedures were used by Duncan, et al. (1985). Suggestions on choice of the available force and its orientation are given in Humphrey and Holtz (1986a). The orientation of the force is specified by the inclination factor I_f . I_f varies from 0.0 which specifies that the force acts in the direction of the reinforcement to 1.0 which specifies that it acts tangent to the slip surface as shown in Fig. 3.

The right most intersection of each reinforcing layer and the trial surface is located. Then the force (F_{Rj}) and inclination factor (I_{fj}) at the intersection is found by linear interpolation between the adjacent specified points (Fig. 2). It is possible for the toe of some trial circles



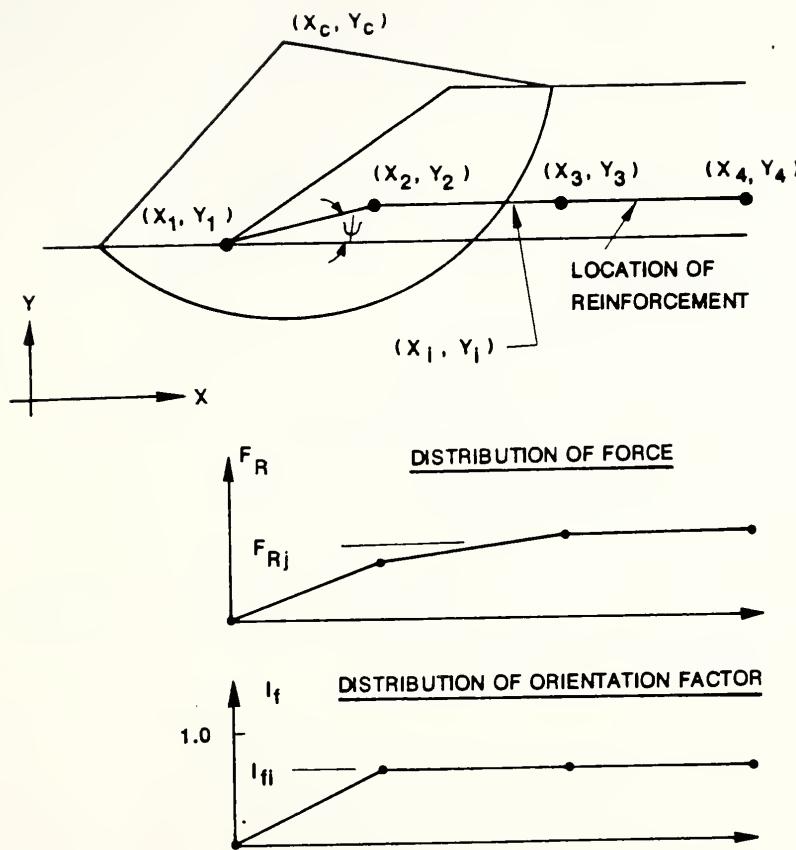


Figure 2 Location of reinforcement and distribution of force and inclination factor.



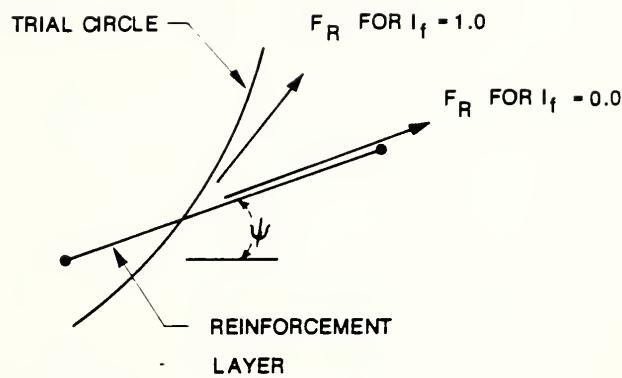


Figure 3 Orientation of reinforcement force.



to intersect a layer a second time but this is assumed to have no effect on stability.

The moment arm (y) is a function of the trial circle radius (r), the slope of the reinforcement (ψ), the inclination factor, the coordinates of the circle center (x_c, y_c), and the coordinates of the intersection (x_i, y_i) as shown on Fig. 2. For a horizontal layer and $I_f = 0.0$, $y = y_c - y_i$ and for $I_f = 1.0$, $y = r$. For other cases

$$A = \text{atan}[(x_c - x_i)/(y_c - y_i)] \quad (2)$$

$$y = r \sin[\pi/2 - A + \psi + I_f(A - \psi)] \quad (3)$$

The reinforcing option is implemented only for the simplified Bishop method. This restricts solution options to SURBIS for a single specified trial circle or CIRCL2 for multiple circles generated using a random technique. An example problem using the SURBIS option is shown in Appendix B. Input instructions are given in Appendix C and error codes are listed in Appendix D.

STABL5 has the capability to analyze many different types of problems. Some combinations of solution options may produce unrealistic results, for example, using the reinforcing and tieback options together. The user should exercise good judgment in this regard.



SUMMARY

A modification to a general purpose slope stability program STABL5 is described which gives it the capability to analyze reinforced embankments constructed on soft ground. The modification is based on the simplified Bishop method of slices. Multiple reinforcing layers with specified distributions of available force may be used. The equations and procedures used in the implementation are given. An example problem, input instructions, error codes, and modifications to STABL5 are given in the appendices.

ACKNOWLEDGEMENTS

Financial support for this research was provided by the Indiana Department of Highways and the Federal Highway Administration through the Joint Highway Research Project of Purdue University. This support is gratefully acknowledged.

APPENDIX A - REFERENCES

Bishop, A. W. (1955), "The use of the slip circle in the stability analysis of slopes," Geotechnique, Vol. 5, No. 1, pp. 7-17.

Boutrup, E. (1978), "Computerized slope stability analysis for Indiana Highways," Masters Thesis, School of Civil Engineering, Purdue University, West Lafayette, Indiana 47907.

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Duncan, J. M., Low, B. K., and Schaefer, V. R. (1985), "STABGM: A computer program for slope stability analysis of reinforced embankments and slopes," Department of Civil Engineering, Virginia Tech, Blacksburg, VA 24061, 28 pp.

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Ingold, T. S. (1982), "An analytical study of geotextile reinforced embankments," Proceedings of the Second International Conference on Geotextiles, Las Vegas, Nevada, August, Vol. III, pp. 683-688.

Lovell, C. W., Sharma, S. S., and Carpenter, J. R. (1984), "Slope stability analysis with STABLE4," Joint Highway Research Report No. JHRP-84-19, School of Civil Engineering, Purdue University, West Lafayette, Indiana 47907.

Siegel, R. A. (1975a), "STABL user manual," Joint Highway Research Report No. JHRP-75-9, School of Civil Engineering, Purdue University, West Lafayette, Indiana 47907.

Siegel, R. A. (1975b), "Computer analysis of general slope stability problems," Masters Thesis, School of Civil Engineering, Purdue University, West Lafayette, Indiana 47907.



APPENDIX B - EXAMPLE PROBLEM

This is a simple example on the use of the reinforcing layer option for a 6-foot high embankment with a 2h:1v side slope as shown in Fig. B-1. The embankment fill is cohesionless with a unit weight of 125 pcf and a friction angle ϕ of 30° . The foundation is soft clay with a unit weight of 115 pcf and an undrained shear strength of 125 psf. The water table is assumed to be very deep. The embankment is reinforced with a single layer located at its base. The available force is specified to be zero at the toe increasing to 500 lb/ft under the central portion of the embankment as shown in Fig. B-1. The force is assumed to act in the direction of the reinforcement so the inclination factor is 0.0. The safety factor is calculated for the trial circle shown in Fig. B-1.

The following input file was prepared using the instructions in Siegel (1975a) and Appendix C. The output for the problem is shown on the following pages. A plot of problem geometry generated using PLOTSTBL.BAS on a Hewlett-Packard 7470A plotter is also shown.



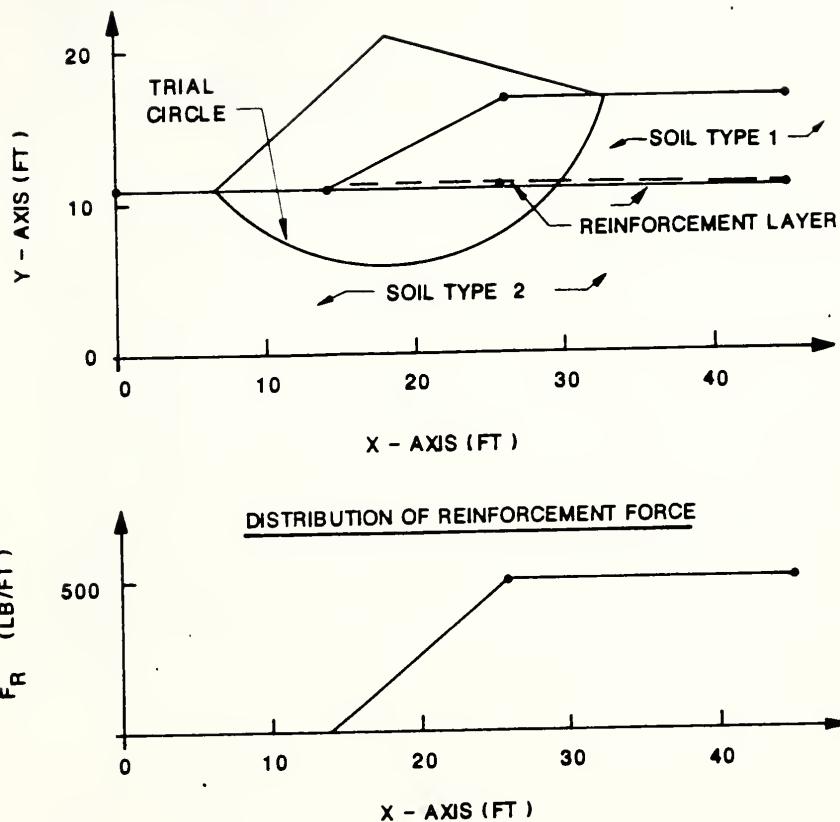


Figure B-1 Example problem.



number of species = 1-5 species

Input for example

```
PROFIL
REINFORCED EMBANKMENT - EXAMPLE
4 3
0. 11. 14. 11. 2
14. 11. 26. 17. 1
26. 17. 45. 17. 1
14. 11. 45. 11. 2
SOIL
2
125. 125. 0. 30. 0. 0. 0
115. 115. 125. 0. 0. 0. 0
REINF
1
3
14. 11. 0. 0.
26. 11. 500. 0.
45. 11. 500. 0.
SURBIS
13
6.00 11.00
8.12 8.88
10.61 7.20
13.37 6.03
16.30 5.40
19.30 5.33
22.26 5.84
25.06 6.90
27.62 8.48
29.83 10.51
31.61 12.92
32.90 15.63
33.25 17.00
EXECUT
```


Output for example

** PCSTABL5 **

by
Purdue University--Slope Stability Analysis--
Simplified Janbu, Simplified Bishop
or Spencer's Method of Slices

Run Date: 6/13/86
 Time of Run: 8:30 PM
 Run By: D. Humphrey
 Input Data Filename: example.in
 Output Filename: example.out
 Plotted Output Filename: example.plt

PROBLEM DESCRIPTION REINFORCED EMBANKMENT - EXAMPLE

BOUNDARY COORDINATES

3 Top Boundaries
 4 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	11.00	14.00	11.00	2
2	14.00	11.00	26.00	17.00	1
3	26.00	17.00	45.00	17.00	1
4	14.00	11.00	45.00	11.00	2

ISOTROPIC SOIL PARAMETERS

2 Type(s) of Soil

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	125.0	125.0	0.0	30.0	0.00	0.0	0
2	115.0	115.0	125.0	0.0	0.00	0.0	0



Output for example (cont.)

REINFORCING LAYER(S)

1 REINFORCING LAYER(S) SPECIFIED

REINFORCING LAYER NO. 1

3 POINTS DEFINE THIS LAYER

POINT NO.	X-COORD	Y-COORD	FORCE	INCLINATION FACTOR
1	14.00	11.00	0.00	0.000
2	26.00	11.00	500.00	0.000
3	45.00	11.00	500.00	0.000

Trial Failure Surface Specified By 13 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	6.00	11.00
2	8.12	8.88
3	10.61	7.20
4	13.37	6.03
5	16.30	5.40
6	19.30	5.33
7	22.26	5.84
8	25.06	6.90
9	27.62	8.48
10	29.83	10.51
11	31.61	12.92
12	32.90	15.63
13	33.25	17.00

Circle Center At X = 18.1 ; Y = 21.0 and Radius, 15.7

Factor Of Safety For The Preceding Specified Surface = 1.079

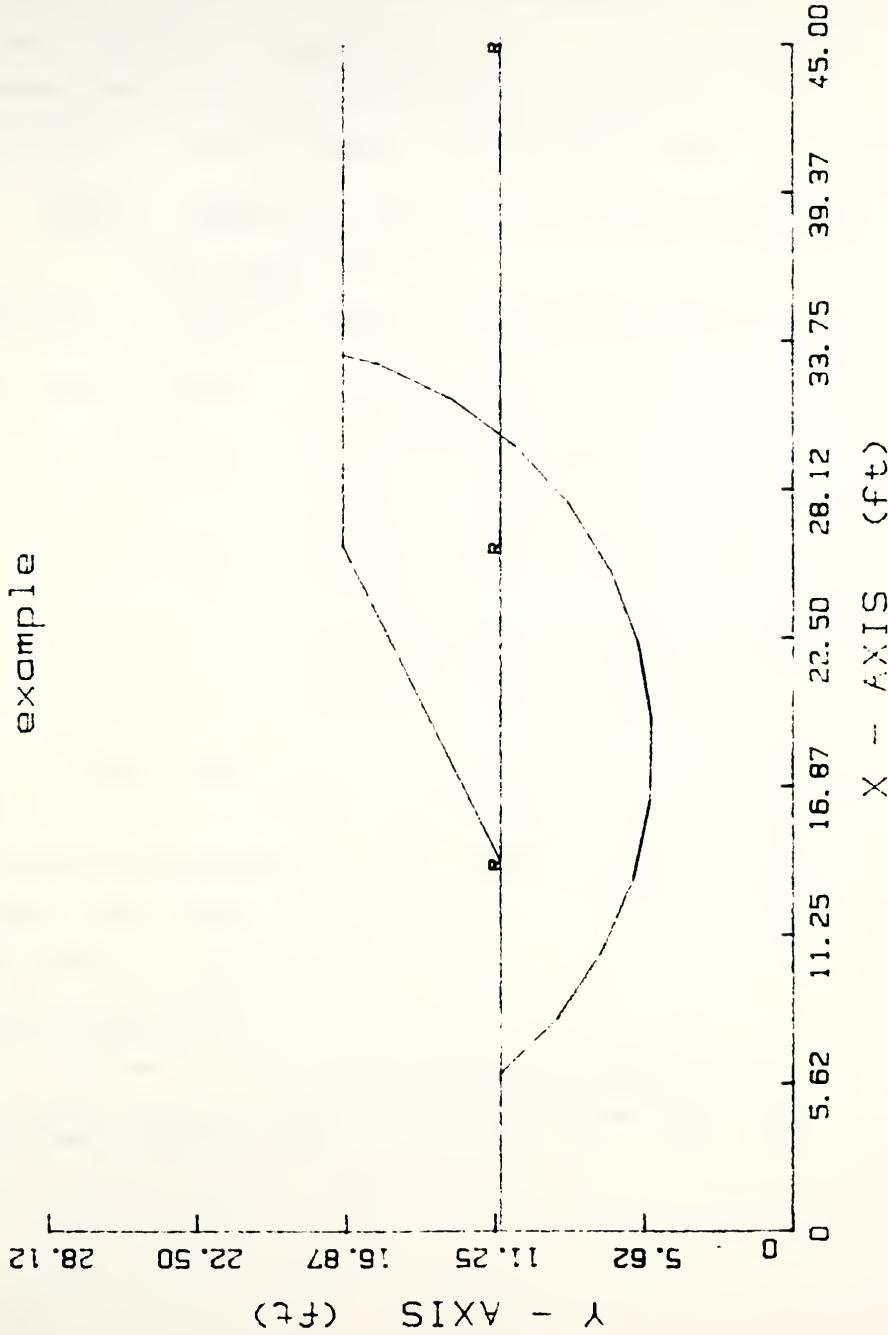
WARNING - Factor Of Safety Is Calculated By The Modified Bishop Method. This Method Is Valid Only If The Failure Surface Approximates A Circle.



Output for example (cont.)

Example plot from Hewlett-Packard 7470A plotter.

example



Comunicação entre pessoas diferentes, entre pessoas de diferentes culturas.

Comunicação

CEFA - BIXA - Y



APPENDIX C - DATA INPUT FORMAT FOR REINFORCING LAYERS

C.1 Input for Reinforcing Layers

COMMAND CARD REINF Command Code

DATA CARD Integer Number of reinforcing layers

NOTE: Repeat the following set of data cards for each reinforcing layer.

DATA CARD Integer Number of points defining the reinforcing layer

DATA CARD Real X coordinate of point on reinforcing layer

Real Y coordinate of point on reinforcing layer

Real Force in reinforcement at point (force/unit width)

Real Inclination factor; between 0.0 and 1.0; = 0.0 force acts in plane of reinforcement; = 1.0 force acts tangent to failure surface

NOTE: Repeat preceding data card for each point defining the reinforcing layer.

C.2 Input for Suppressing or Reactivating Reinforcing Layers

COMMAND CARD REINF Command Code

DATA CARD Integer Number zero (0)

C.3 Input Restrictions

1. No more than 10 reinforcing layers can be specified.
2. A reinforcing layer must be specified by at least 2 but not more than 40 points.
3. The reinforcing force must be positive.



4. The inclination factor must be between 0.0 and 1.0. A factor of 0.0 specifies that the reinforcing force acts in the direction of the reinforcement. A factor of 1.0 specifies that the force acts tangent to the failure surface.

APPENDIX D - REINF ERROR CODES

- RF01 - An attempt has been made to suppress or reactivate undefined reinforcing layers. Data must be defined by prior use of command REINF before they can be suppressed. Suppressed data can not be reactivated if command PROFIL has been used in the execution sequence subsequent to use of REINF, whether the data are active or suppressed.
- RF02 - The number of reinforcing layers specified exceeds 10. The problem must either be redefined so fewer reinforcing layers are used or dimensioning of the program must be increased to accommodate the problem as defined.
- RF03 - The number of points defining a reinforcing layer exceeds 40. The problem must be either redefined so fewer points are used or the dimensioning of the program must be increased to accommodate the problem as defined.
- RF04 - A negative coordinate has been specified for the reinforcing layer and point number indicated. All problem geometry must be located within the first quadrant.
- RF05 - A negative reinforcing force has been specified for the reinforcing layer and point number indicated. The reinforcing force must be zero or positive.
- RF06 - An inadmissible inclination factor has been specified for the reinforcing layer and point number indicated. The inclination factor must be between 0.0 and 1.0.
- RF07 - The reinforcing layer and point number indicated is not to the right of the points specified prior to it. The points defining the reinforcing layer must be specified in left to right order.
- RF08 - The reinforcing layer indicated is specified by only one point. The reinforcing layer must be specified by at least two points.
- RF09 - An attempt has been made to use the reinforcing layer option with the simplified Janbu method of analysis. The reinforcing layer option can only be used with the simplified Bishop method of analysis.



APPENDIX E - MODIFICATIONS TO PC-STABL5

This appendix describes modifications made to PC-STABL5 which was originally compatible with Microsoft FORTRAN, Version 3.21 (MS-FORTRAN). The modifications were made for two reasons. The first were changes to make the program compatible with Ryan-McFarland, Version 2.00 FORTRAN (RM-FORTRAN). These were mostly minor such as commas in format statements and are listed below. In addition, MS-FORTRAN uses a special \$NOFLOATCALLS statement at the beginning of each program unit; these were made inactive in the RM-FORTRAN version by substituting CNOFLOATCALLS. The MS-FORTRAN version writes program output simultaneously to a file (unit 6) and to the screen (unit *). This was done with two WRITE statements, one for each unit. This scheme is not compatible with RM-FORTRAN since it treats unit 6 and unit * as the same unit. To eliminate the problem all WRITE statements to unit * were made inactive by inserting 'c **' in columns 1-4. The second reason for the changes was to incorporate the reinforcing layer option. The modifications are listed below. They included minor modifications to several existing subroutines and the addition of two new subroutines.



Modifications to main program STABL5

```

Add after stbl 12
c 1986 Modifications for reinforcing layer option (PCSTABL6)
c
c      Dana N. Humphrey, Graduate Research Assistant, May 1986.
c
Add after stbl 160
    common /blk23/ireinf,nreinf,nrpnts(10),xreinf(10,40),
    ^           yreinf(10,40),rforce(10,40),rincif(10,40),rmoms
Add after stbl 168
    real load,limit,kcoef,inclin,length
    integer sitp,bn
Replace existing Jrcmay85 following stbl 172 with
    1 'LIMITS','ANISO','SURBIS','SPENCR','REINF'
Add after stbl 200
    ireinf=0
    rmoms=0.
Replace existing Jrcmay85 following stbl 324 with
    23 do 12 i=1,18
Replace existing Jrcmay85 following stbl 328 with
    1 13,30,35),1
Replace existing Jrcmay85 following stbl 350 with
c *** write(*,102)(keyw(i),i=1,18)
    write(6,102)(keyw(i),i=1,18)
Add after stbl 510
    35 call reinf
        go to 11

```

Modifications to subroutine BLOCK2

Add after blk2 56
real limit

Modifications to subroutine EXECUT

```
Add before exec 46
    common /b1k23/ireinf,nreinf,nrpts(10),xreinf(10,40),
           yreinf(10,40),rforce(10,40),rincf(10,40),rmoms      dnhmav86
dnhmav86
Add after exec 62
    if(ireinf.eq.1)call reinf2                                dnhmav86
```

Modifications to subroutine FACTR

```
Add after fctr 148
    common /blk23/ireinf,nreinf,nrpts(10),xreinf(10,40),
           ^          yreinf(10,40),rforce(10,40),rincif(10,40),rmoms
dnhmay86
dnhmay86
Recpace existing fctr 296 with
    do 10 j=1,20
dnhlu186
```


Replace existing fctr 314 with
 if(irelinf.eq.1)then
 bottom=sumb-rmoms/(radius*fold)
 if(bottom.gt.0.)then
 fnew= sumt/bottom
 fnew=(fold+fnew)/2.
 else
 fnew=2.*fold
 endif
 else
 fnew= sumt/sumb
 endif

Add after fctr 322
 foldx=fold

Replace existing fctr 338 with
 110x,'Factor Of Safety Calculation Has Gone Through 20 Iterations'

Replace existing fctr 346 and 348 with
 if(isearc.eq.0) write(6,108)fs,foldx
 c *** if(isearc.eq.0) write(*,108)fs,foldx
 108 format(//10x,'Factor of Safety for the Preceding Surface is ',
 1 'Between',f6.3,', and',f6.3)

Replace existing fctr 374 and 376 with
 write(6,108)fs,foldx
 c *** write(*,108)fs,foldx

Add before fctr 386
 rmoms=0.

Replace existing fctr 414 with
 110x,'*** The Above Factor Of Safety Is Misleading ***')

Replace existing fctr 430 through 438 with
 110x,'The Factor Of Safety For The Trial Failure Surface Defined'/
 110x,'By The Coordinates Listed Below Is Misleading.'///
 110x,'Failure Surface Defined By',i3,' Coordinate Points'///
 112x,'Point',6x,'X-Surf',6x,'Y-Surf',/
 113x,'No.',8x,'(ft)',8x,'(ft)',//)

Modifications to subroutine FSPENC

Replace existing fspn 726 with
 110x,'*** The Above Factor Of Safety Is Misleading ***')

Replace existing fspn 742 through fspn 750 with
 110x,'The Factor Of Safety For The Trial Failure Surface Defined'/
 110x,'By The Coordinates Listed Below Is Misleading.'///
 110x,'Failure Surface Defined By',i3,' Coordinate Points'///
 112x,'Point',6x,'X-Surf',6x,'Y-Surf',/
 113x,'No.',8x,'(ft)',8x,'(ft)',//)

Replace existing fspn 780 and fspn 782 with
 201 write(6,202)
 c *** write(*,202)

Modifications to subroutine PLOTIN

Add after plot 62

```
common /blk23/ireinf,nreinf,nrpts(10),xreinf(10,40),
      ^          yreinf(10,40),rforce(10,40),rincf(10,40),rmoms
```

dnhmay86
dnhmay86

Replace existing plot 66 with

dimension plttr(11)

dnhmay86

Replace existing plot 76 with

1 'SRF','TEN','RNF','NPL','END' /

dnhmay86

Replace existing plot 96 with

write(7,100)plttr(10)

dnhmay86

Add after plot 376

```
c -----
c   plot reinforcing layers, if applicable
c -----
```

dnhmay86
dnhmay86
dnhmay86

3 if(ireinf.eq.0)go to 49

write(7,100)plttr(9)

dnhmay86
dnhmay86

write(7,113)nreinf

dnhmay86

do 45 n=1,nreinf

dnhmay86

write(7,113)nrpts(n)

dnhmay86

x=xreinf(n,1)/scle

dnhmay86

y=yreinf(n,1)/scle

dnhmay86

write(7,115)x,y

dnhmay86

nn=nrpts(n)

dnhmay86

do 45 i=2,nn

dnhmay86

x=xreinf(n,i)/scle

dnhmay86

y=yreinf(n,i)/scle

dnhmay86

write(7,115)x,y

dnhmay86

45 continue

dnhmay86

Replace existing plot 384 with

49 if(iblk.eq.0)go to 9

dnhmay86

Modifications to subroutine PLTN

Add after pltin 62

```
common /blk23/ireinf,nreinf,nrpts(10),xreinf(10,40),
      ^          yreinf(10,40),rforce(10,40),rincf(10,40),rmoms
```

dnhmay86
dnhmay86

Replace existing pltin 64 with

dimension plt(49,51),symb(21),axis(9),sc1(9)

dnhmay86

Add after pltin 66

real load,inclin,length

dnhmay86

integer bn

dnhmay86

Add after pltin 68

character plt*1

dnhmay86

Replace existing pltin 72 with

1 'W','L','S','.', '/', 'T','R' /

dnhmay86

Add after pltin 366

```
c -----
c   position points defining reinforcing layers, if applicable
c -----
```

dnhmay86
dnhmay86
dnhmay86

10 if(ireinf.eq.0)go to 39

dnhmay86

do 36 i=1,nreinf

dnhmay86

nn = nrpts(i)

dnhmay86


```
      do 36 j=1,nm
      call postn(xreinf(i,j),yreinf(i,j),ix,iy)
      plt(ix-1,iy)=symb(1)
      plt(ix,iy)=symb(21)
 36 continue
Replace existing plt 374 with
 39 do 8 i=1,nbnd
```

Modifications to subroutine PROFIL

Modifications to subroutine RANDOM

Replace existing rand 620 with
110x,'Sliding Block Is',f6.1,//)

Modifications to subroutine READER

Add after read 46
character m*| dnbmax86

Modifications to subroutine SCALER

Add after scal 64
real load,inclin,length
integer bn

Modifications to subroutine SLICES

Add before slice S0
real load

Modifications to subroutine SOILWT

Modifications to subroutine TIES

Replace existing ties 222 with

105 format(/,10x,14h**** ERROR - ,a4,6h ****,5x,4hTie ,13,/) dnhmay86

Modifications to subroutine TRANS

Add after tran 68

integer sltp dnhmay86

Modifications to subroutine WEIGHT

Replace existing 11ines wght 200 through wght 208 with

110x,*****'/ dnhmay86
110x,***** INPUT ERROR - Trial Failure Surface *****'/ dnhmay86
110x,***** Extends Above The *****'/ dnhmay86
110x,***** Ground Surface *****'/ dnhmay86
110x,*****') dnhmay86New subroutine REINF

```

SUBROUTINE REINF
C -----
C -----
C          SUBROUTINE REINF
C -----
C -----
C          FUNCTIONS -
C
C          READ THE NUMBER OF REINFORCING LAYERS.
C
C          IF EQUAL TO ZERO, EXISTING REINFORCING LAYER DATA IS SUPPRESSED
C          OR REACTIVATED IF PREVIOUSLY SUPPRESSED.
C
C          IF GREATER THAN ZERO, READS, CHECKS, STORES, AND PRINTS
C          REINFORCING LAYER DATA.
C
C -----
C -----
C
CNOFLOATCALLS
COMMON /BLK01/IANGL,IBLK,IEXIT,ICIRC,ILIMIT,IPLOT,IREAD,ISEARC,
I           IBLK2,ISOIL,ISTR,ISURC,ISURF,ITIES,IWAT,RD,TOL,
I           CBLK,CPLT
COMMON /BLK23/IREINF,NREINF,NRPTS(10),XREINF(10,40),
I           YREINF(10,40),RFORCE(10,40),RINCLF(10,40),RMOMS
DIMENSION ERROR(8)
CHARACTER ERROR*4
DATA ERROR/'RF01','RF02','RF03','RF04','RF05','RF06','RF07',
I           'RF08'/
```



```
C -----  
C READ NUMBER OF REINFORCING LAYERS  
C -----  
C CALL READER(DUMMY,NREIN,0)  
C -----  
C CHECK FOR REINFORCING LAYER DATA SUPPRESSION  
C -----  
IF(NREIN.EQ.0) THEN  
  IF(IREINF.NE.0) THEN  
    IREINF=0  
C ***  WRITE(*,108)  
    WRITE(6,108)  
108  FORMAT(///,  
           10X,'REINFORCING LAYER DATA LAYER DATA HAS BEEN SUPPRESSED')  
C -----  
C CHECK IF DATA DEFINED BEFORE REACTIVATING IT  
C -----  
ELSE IF(NREINF.EQ.0) THEN  
C ***  WRITE(*,101)ERROR(1)  
    WRITE(6,101)ERROR(1)  
101  FORMAT(/,10X,14H*** ERROR - ,A4,6H ****,/)  
    IEXIT=1  
C -----  
C REACTIVATE SUPPRESSED DATA  
C -----  
ELSE  
  IREINF=1  
C ***  WRITE(*,109)  
    WRITE(6,109)  
109  FORMAT(///,  
           10X,'SUPPRESSED REINFORCING LAYER DATA HAS BEEN REACTIVATED')  
  ENDIF  
  RETURN  
ENDIF  
NREINF=NREIN  
IREINF=1  
C -----  
C PRINT NUMBER OF REINFORCING LAYERS  
C -----  
C *** WRITE(*,103)NREINF  
    WRITE(6,103)NREINF  
103 FORMAT(1H1,  
           ^///,9X,'REINFORCING LAYER(S)',//,  
           ^ 13X,12,' REINFORCING LAYER(S) SPECIFIED')  
C -----  
C CHECK REINFORCING LAYER STORAGE LIMIT  
C -----  
IF(NREINF.GT.10)THEN  
C ***  WRITE(*,101)ERROR(2)  
    WRITE(6,101)ERROR(2)  
    CALL QUIT  
  ENDIF  
  DO 20 I=1,NREINF  
C -----
```



```

C READ NUMBER OF POINTS DEFINING LAYER
C -----
C           CALL READER(DUMMY, NRPTS(I),0)
C -----
C CHECK FOR AT LEAST TWO POINTS
C -----
C           IF(NRPTS(I).LT.2)THEN
C ***      WRITE(*,101)ERROR(8)
C           WRITE(6,101)ERROR(8)
C           IEXIT=1
C           ENDIF
C -----
C CHECK POINT STORAGE LIMIT
C -----
C           IF(NRPTS(I).GT.40)THEN
C ***      WRITE(*,101)ERROR(3)
C           WRITE(6,101)ERROR(3)
C           CALL QUIT
C           ENDIF
C -----
C PRINT REINFORCING LAYER DATA HEADINGS
C -----
C ***      WRITE(*,102) I,NRPTS(I)
C           WRITE(6,102) I,NRPTS(I)
102  FORMAT(///,
     ^ 10X,'REINFORCING LAYER NO. ',I3//,
     ^ 10X,I3,' POINTS DEFINE THIS LAYER',//,
     ^ 15X,'POINT ',5X,'X-COORD',3X,'Y-COORD',3X,'FORCE',3X,
     ^ 'INCLINATION',
     ^ 16X,'NO.',36X,'FACTOR')
C -----
C READ AND CHECK REINFORCING LAYER DATA
C -----
C           XP=-TOL
C           YP=-TOL
C           DO 10 N=1,NRPTS(I)
C           CALL READER(XREINF(I,N),IDUMMY,I)
C           CALL READER(YREINF(I,N),IDUMMY,I)
C           CALL READER(RFORCE(I,N),IDUMMY,I)
C           CALL READER(RINCLF(I,N),IDUMMY,I)
C -----
C CHECK FOR 1ST QUADRANT LOCATION
C -----
C           IF(XREINF(I,N).LE.-TOL .OR. YREINF(I,N).LE.-TOL)THEN
C ***      WRITE(*,104)ERROR(4),I,N
C           WRITE(6,104)ERROR(4),I,N
104  FORMAT(/,10X,14H*** ERROR - ,A4,6H ****,5X,
     ^ 'LAYER NO.',I3,5X,'POINT NO.',I3)
     ^ IEXIT=1
C           ENDIF
C -----
C CHECK FOR POSITIVE REINFORCING FORCE
C -----
C           IF(RFORCE(I,N).LE.-TOL)THEN

```



```

C ***      WRITE(*,104)ERROR(5),I,N
C           WRITE(6,104)ERROR(5),I,N
C           IEXIT=1
C           ENDIF
C -----
C   CHECK LIMITS OF INCLINATION FACTOR
C -----
C ***      IF(RINCLF(I,N).LE.-TOL .OR. RINCLF(I,N).GT.I.+TOL)THEN
C           WRITE(*,104)ERROR(6),I,N
C           WRITE(6,104)ERROR(6),I,N
C           IEXIT=1
C           ENDIF
C -----
C   CHECK FOR POSITIVE SPACING
C -----
C ***      IF(XREINF(I,N).LT.XP .OR. YREINF(I,N).LT.YP)THEN
C           WRITE(*,104)ERROR(7),I,N
C           WRITE(6,104)ERROR(7),I,N
C           IEXIT=1
C           ENDIF
C           XP=XREINF(I,N)
C           YP=YREINF(I,N)
10    CONTINUE
C -----
C   PRINT REINFORCING LAYER DATA
C -----
C ***      WRITE(*,106) (N,XREINF(I,N),YREINF(I,N),RFORCE(I,N),RINCLF(I,N),
C ***^   N=1,NRPTS(I))
C           WRITE(6,106) (N,XREINF(I,N),YREINF(I,N),RFORCE(I,N),RINCLF(I,N),
C           ^   N=1,NRPTS(I))
106   FORMAT(15X,13,3X,3F10.2,F10.3)
20    CONTINUE
      RETURN
      END

```

New subroutine REINF2

```

      SUBROUTINE REINF2
C -----
C -----
C           SUBROUTINE REINF2
C -----
C -----
C   FUNCTIONS -
C
C     LOCATES INTERSECTION BETWEEN TRIAL SURFACE AND REINFORCING
C     LAYER(S).
C
C     CALCULATES RESISTING MOMENT PROVIDED BY REINFORCING LAYER(S).
C
C -----

```



```

C
CNOFLOATCALLS
  COMMON /BLK01/IANGL,IBLK,IEXIT,ICIRC,ILIMIT,IPLOT,IREAD,ISEARC,
  I           IBLK2,ISOIL,ISTR,ISURC,ISURF,ITIES,IWAT,RD,TOL,
  I           CBLK,CPLT
  COMMON /BLK05/NSURF,SURF(100,2)
  COMMON /BLK15/M,MB
  COMMON /BLK22/RADIUS
  COMMON /BLK23/IREINF,NREINF,NRPTS(10),XREINF(10,40),
  ^           YREINF(10,40),RFORCE(10,40),RINCLF(10,40),RMOMS
  DIMENSION ERROR(1)
  CHARACTER ERROR*4
  DATA ERROR/'RF09'/

C -----
C C CHECK THAT MODIFIED BISHOPS METHOD SPECIFIED
C -----
C
C *** IF(MB.NE.1)THEN
C ***   WRITE(*,101)ERROR(1)
C ***   WRITE(6,101)ERROR(1)
101  FORMAT(/,10X,14H*** ERROR - ,A4,6H ***,/)
  CALL QUIT
  ENDIF
  RMOMS=0.

C -----
C C CHECK FOR INTERSECTION AND CALCULATE RESISTING
C C MOMENT FOR EACH REINFORCING LAYER
C -----
C
C DO 30 I=1,NREINF
C -----
C C LOCATE INTERSECTION BETWEEN TRIAL SURFACE AND REINFORCING LAYER
C -----
C
  NRPTSI=NRPTS(1)
  DO 10 J=NRPTSI,2,-1
    JI=J-1
    DO 10 K=NSURF,2,-1
      KI=K-1
      CALL INTSCT(XREINF(I,JI),YREINF(I,JI),XREINF(I,J),
      ^           YREINF(I,J),SURF(KI,1),SURF(KI,2),SURF(K,1),SURF(K,2),
      ^           XINT,YINT,INTS)
      IF(INTS.EQ.1) GOTO 20
10  CONTINUE
C -----
C C IF NO INTERSECTION GO TO NEXT REINFORCING LAYER
C -----
C
  GOTO 30
C -----
C C INTERPOLATE REINFORCING FORCE AND INCLINATION FACTOR AT INTERSECTION
C -----
C
20  FAC=(XREINF(I,JI)-XINT)/(XREINF(I,J1)-XREINF(I,J))
  RFORCI=RFORCE(I,J1)+FAC*(RFORCE(I,J)-RFORCE(I,J1))
  RINCLI=RINCLF(I,J1)+FAC*(RINCLF(I,J)-RINCLF(I,J1))
C -----
C C FOR FORCE TANGENT TO CIRCLE MOMENT ARM EQUALS RADIUS
C -----

```



```

IF(RINCL1.GE.1.-TOL)THEN
  RARM=RADIUS
ELSE
C -----
C CALCULATE CENTER OF CIRCLE
C -----
  X1=SURF(1,1)
  Y1=SURF(1,2)
  X2=SURF(2,1)
  Y2=SURF(2,2)
  X3=SURF(3,1)
  Y3=SURF(3,2)
  XHALF2=(X2 + X3)/2.0
  YHALF2=(Y2 + Y3)/2.0
  XCNTR=((X1**2-X2**2)*(Y3-Y2) - (X2**2-X3**2)*(Y2-Y1) + (Y3-Y1)
  1   *(Y2-Y1)*(Y3-Y2))/(2.0*((X1-X2)*(Y3-Y2) - (X2-X3)*
  2   (Y2-Y1)))
  YCNTR=(X2-X3)/(Y3-Y2)*(XCNTR - XHALF2) + YHALF2
C -----
C CALCULATE MOMENT ARM FOR FORCE NOT TANGENT TO CIRCLE
C -----
  A1=ATAN((YREINF(I,J)-YREINF(I,JI))/(XREINF(I,J)-XREINF(I,JI)))
  A2=ATAN((XINT-XCNTR)/(YCNTR-YINT))
  A3=A1+RINCL1*(A2-A1)
  A4=1.570796327-A2+A3
  RARM=RADIUS*SIN(A4)
ENDIF
C -----
C CALCULATE AND SUM RESISTING MOMENT
C -----
  RMOM=RFORC1*RARM
  RMOMS=RMOMS+RMOM
30 CONTINUE
  RETURN
  END

```


APPENDIX F - LIST OF ADDITIONS AND MODIFICATIONS TO PLOTSTBL.BAS

The modifications which were made to PLOTSTBL.BAS to give it the capability to plot the location of reinforcing layers are listed below. An 'A' in the first column indicates that the line should be added to the existing program and 'R' indicates that the line should replace the existing line.

Modifications to PLOTSTBL.BAS

```
R 530 DIM PLT$(11)
R 730 FOR I=1 TO 11
R 1090 FOR J=1 TO 11
R 1110 ON J GOTO 1140,1360,1570,1750,1940,2152,2310,2450,2131,2600,2700
A 2131 REM -----
A 2132 REM PLOT REINFORCING LAYERS, IF APPLICABLE
A 2133 REM -----
A 2134 IF PROMPT$="y" THEN GOSUB 2900
A 2135 INPUT #2,NREINF%
A 2136 FOR I=1 TO NREINF%
A 2137 INPUT #2,NN%
A 2138 GOSUB 2830
A 2139 PRINT #1, "PU,PA";X#,Y#;
R 2140 PRINT #1, "SI.15,.2"
A 2141 PRINT #1, "CP-.5,0;D1;LBR"+CHR$(3)
A 2142 PRINT #1, "PU,PA";X#,Y#;
A 2143 FOR J=2 TO NN%
A 2144 GOSUB 2830
A 2145 GOSUB 2770
A 2146 PRINT #1, "CP-.5,0;D1;LBR"+CHR$(3)
A 2147 PRINT #1, "PU,PA";X#,Y#;
A 2148 NEXT J
A 2149 NEXT I
R 2150 GOSUB 2770
A 2151 GOTO 1130
A 2152 REM -----
A 2153 REM PLOT SEARCH BOXES FOR BLOCK, IF APPLICABLE
R 2950 FOR JJ=1 TO 9
R 2970 ON J GOSUB 3000,3030,3060,3090,3120,3150,3180,3210,3241
A 3241 INPUT "SELECT PEN FOR PLOTTING REINFORCING LAYERS (1 OR 2) ";XX
A 3242 GOSUB 3250
A 3243 RETURN
A 3401 DATA RNF
```


COVER DESIGN BY ALDO GIORGINI